

An update on the Eulerian formulation for the simulation of soft solids in fluids

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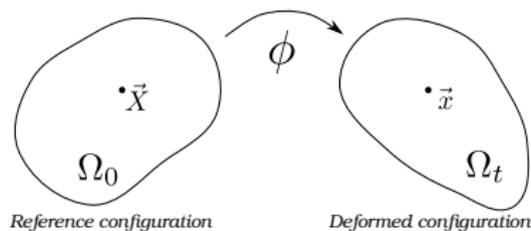


Introduction and Motivation

- System of soft solids in a fluid are ubiquitous
 - Animal tissues, cell membrane.
- Studied for decades - arbitrary Lagrangian-Eulerian (ALE) method - Stiff solids.
- **Need for a fully Eulerian approach with “true solid constitutive laws”.**
 - Eulerian Godunov method (Miller & Colella 2001) - unbounded domains
 - **Reference Map Technique (RMT)** (Kamrin et al. 2012)



Reference Map Technique



Reference map

$$\vec{\xi}(\vec{x}, t) = \vec{X}$$

$$\frac{D\vec{\xi}(\vec{x}, t)}{Dt} = 0 \quad \Rightarrow \quad \frac{\partial \vec{\xi}(\vec{x}, t)}{\partial t} + \vec{u} \cdot \vec{\nabla} \vec{\xi}(\vec{x}, t) = 0$$

Deformation gradient

$$\mathbb{F}(\vec{X}, t) = \partial \vec{x} / \partial \vec{X} = (\vec{\nabla}_{\vec{X}} \vec{\xi}(\vec{x}, t))^{-1}$$

[Valkov et al., *J. Appl. Mech.*, 82, 2015].

Governing equations for solids and fluids

Momentum balance

$$\frac{\partial(\rho\vec{u})}{\partial t} + \nabla \cdot (\rho\vec{u} \otimes \vec{u}) = \nabla \cdot \underline{\underline{\sigma}}$$

Mass balance

Fluid:

$$\frac{\partial\rho}{\partial t} + \vec{\nabla} \cdot (\vec{u}\rho) = 0 \quad \Rightarrow \quad \vec{\nabla} \cdot \vec{u} = 0$$

Solid:

$$\rho = \rho_o(\det(\mathbb{F}))^{-1} \quad \Rightarrow \quad \det(\mathbb{F}) = 1$$

Cauchy stress

Newtonian fluid:

$$\underline{\underline{\sigma}}^f = \mu \left[(\vec{\nabla}\vec{u}) + (\vec{\nabla}\vec{u})^T \right] - \mathbf{1} (\vec{\nabla}P)$$

Neo-Hookean solid:

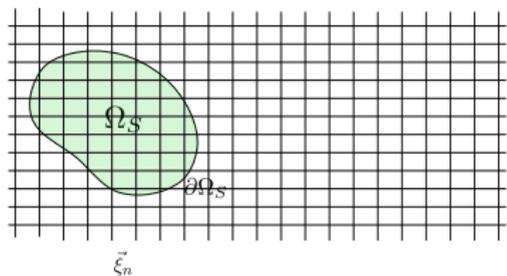
$$\underline{\underline{\sigma}}^s = 2(\det\mathbb{F})^{-1}\mathbb{F} \frac{\partial\hat{\psi}(\mathbb{C})}{\partial\mathbb{C}} \mathbb{F}^T$$

$$\hat{\psi}(\mathbb{C}) = \mu[\text{tr}\mathbb{C} - 3] \quad \Rightarrow \quad \underline{\underline{\sigma}}^s = 2\mu^s [(\vec{\nabla}\vec{\xi})^T (\vec{\nabla}\vec{\xi})]^{-1}$$

[Valkov et al., *J. Appl. Mech.*, 82, 2015].

Basic methodology

$\vec{\xi}$ defined only within the solid.

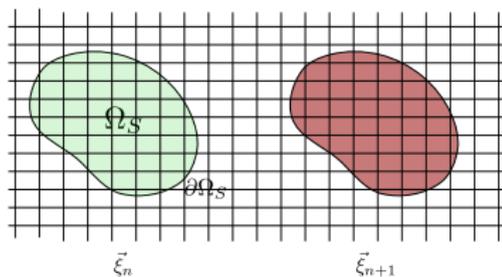


[Valkov et al., *J. Appl. Mech.*, 82, 2015].

Basic methodology

Procedure:

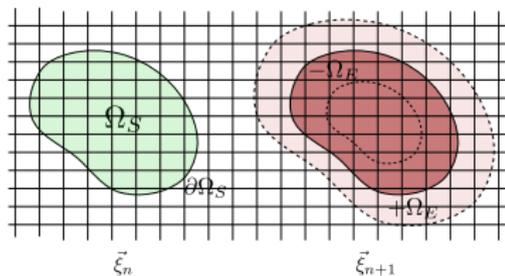
- Solve for $\vec{\xi}_{n+1}$ in Ω_S .



Basic methodology

Procedure:

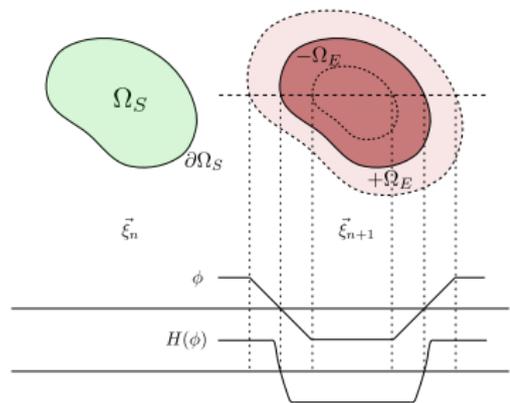
- Solve for $\vec{\xi}_{n+1}$ in Ω_S .
- $\vec{\xi}_{n+1} \rightarrow$ Extrapolate outside Ω_S .



Basic methodology

Procedure:

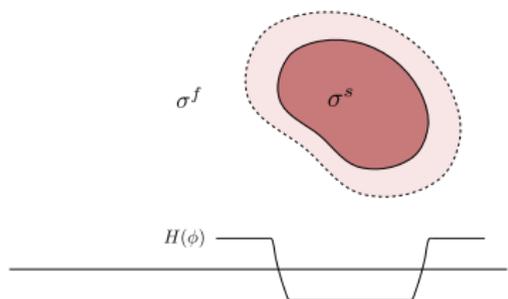
- Solve for $\vec{\xi}_{n+1}$ in Ω_S .
- $\vec{\xi}_{n+1} \rightarrow$ Extrapolate outside Ω_S .
- $\vec{\xi}_{n+1} \rightarrow$ Construct $\phi \rightarrow$ Construct $H(\phi)$.



Basic methodology

Procedure:

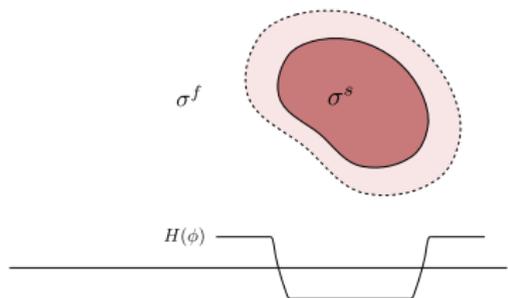
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- Compute $\underline{\underline{\sigma}}^s, \underline{\underline{\sigma}}^f$.



Basic methodology

Procedure:

- Solve for $\vec{\xi}_{n+1}$ in Ω_S .
- $\vec{\xi}_{n+1} \rightarrow$ Extrapolate outside Ω_S .
- $\vec{\xi}_{n+1} \rightarrow$ Construct $\phi \rightarrow$ Construct $H(\phi)$.
- Compute $\underline{\underline{\sigma}}^s, \underline{\underline{\sigma}}^f$.
- $\underline{\underline{\sigma}} \leftarrow$ Blend $f(H(\phi), \underline{\underline{\sigma}}^s, \underline{\underline{\sigma}}^f)$
- $\underline{\underline{\sigma}} \rightarrow$ Compute $\vec{u} \rightarrow$ Project $\vec{\nabla} \cdot \vec{u} = 0$.



Closure model

Fluid-Solid coupling is based on the “*one-fluid formulation*”.

Smoothed heaviside function

$$H(x) = \begin{cases} 0 & x \leq -w_T \\ \frac{1}{2} \left(1 + \frac{x}{w_T} + \frac{1}{\pi} \sin\left(\frac{\pi x}{w_T}\right) \right) & |x| < w_T \\ 1 & x \geq w_T \end{cases}$$

constructed based on the reinitialized level-set field.

Mixture model

$$\underline{\underline{\sigma}} = H(\phi(\vec{x}, t)) \underline{\underline{\sigma}}^f + (1 - H(\phi(\vec{x}, t))) \underline{\underline{\sigma}}^s$$

$$\rho = H(\phi(\vec{x}, t)) \rho^f + (1 - H(\phi(\vec{x}, t))) \rho^s$$

Capability to handle Solid-solid and solid-wall contact.

Updates and major issues fixed

- Momentum conservation - conservative form of equations.

$$\frac{\partial \rho \vec{u}}{\partial t} + \vec{\nabla} \cdot (\rho \vec{u} \vec{u}) = \vec{\nabla} \cdot \left(\sum_i \underline{\underline{\sigma}}_i \right)$$

- Non-dissipative schemes - stress evaluation, convective flux evaluation.
 - Central difference schemes
 - No viscous damping in the solid
- Modified reference map equation - momentum consistent solid advection.
 - Improved robustness

$$\frac{\partial \vec{\xi}(\vec{x}, t)}{\partial t} + H(\psi) \vec{u} \cdot \vec{\nabla} \vec{\xi}(\vec{x}, t) = 0$$

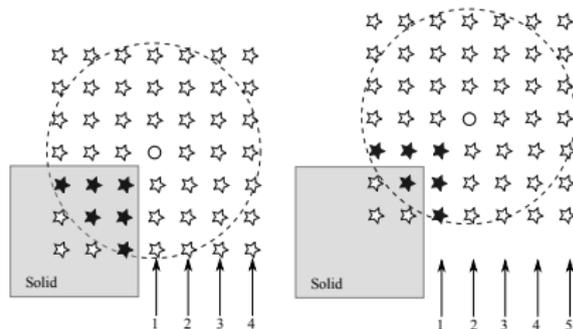
- Least-squares based extrapolation method.
- Collocated grid.

[Jain & Mani, *CTR Annual Research Briefs*, 2017]

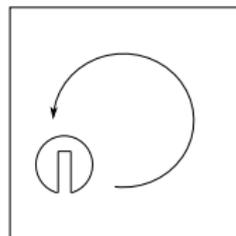
Least-square method for extrapolation

Locally linear approximation

$$\xi = ax + by + c$$



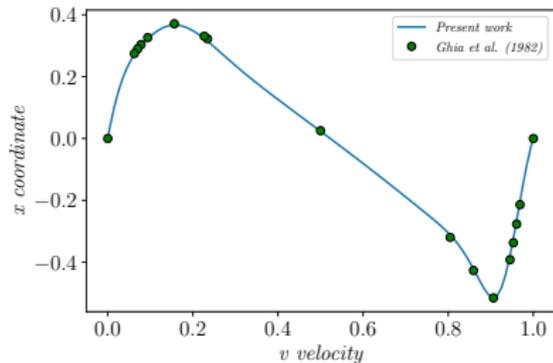
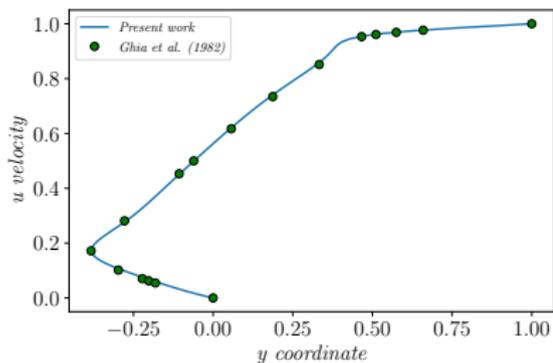
	PDE	least-squares
Error (L_2)	8.32×10^{-4}	6.72×10^{-9}
Cost	$\approx 1550\text{ms}$	$\approx 100\text{ms}$



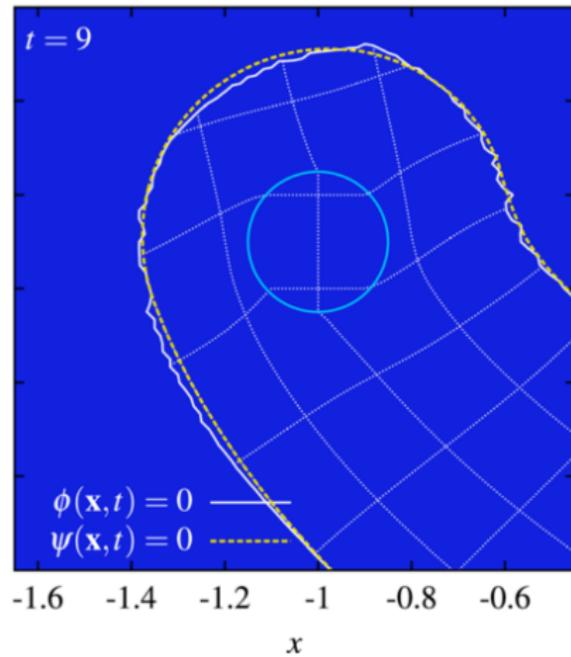
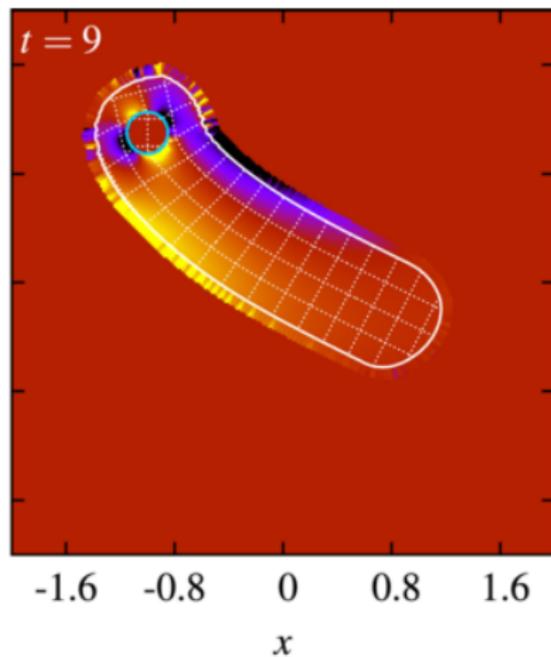
Zalesak disk

Lid-driven cavity

- $Re = 1000$
- 100x100 grid.

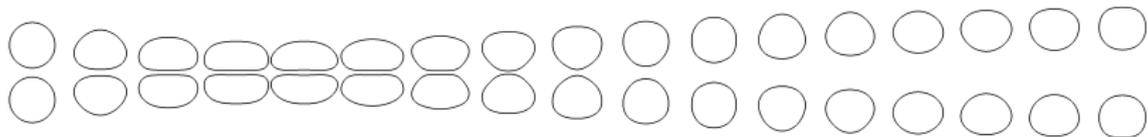
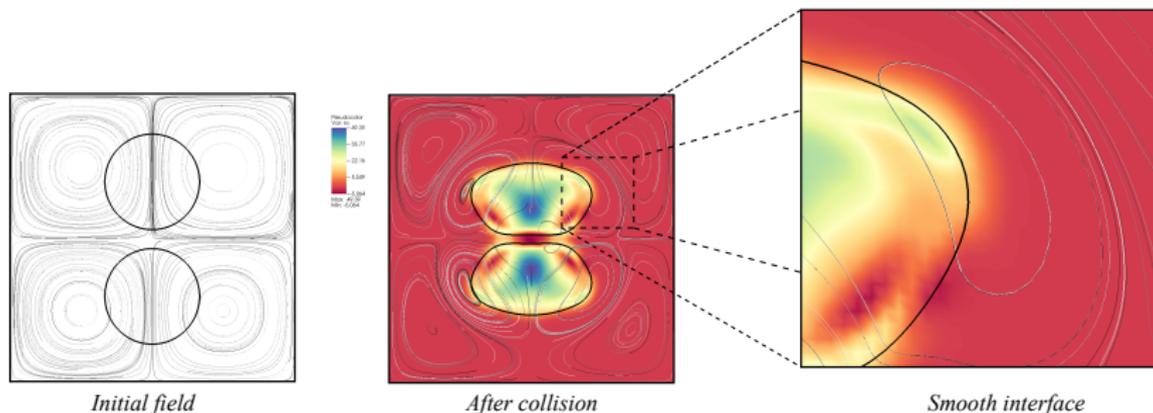


Problems with advecting level-set field



[Valkov et al., 2015]

Two solids in a Taylor-Green Vortex

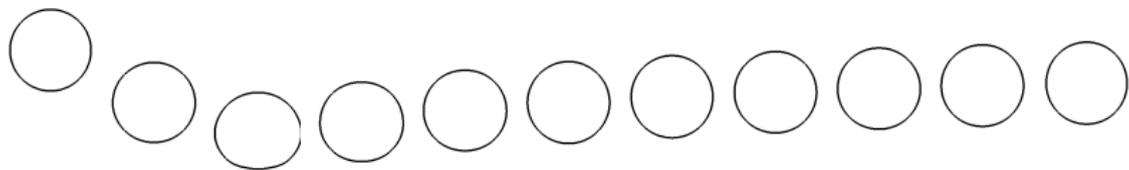


Modified reference map advection equation

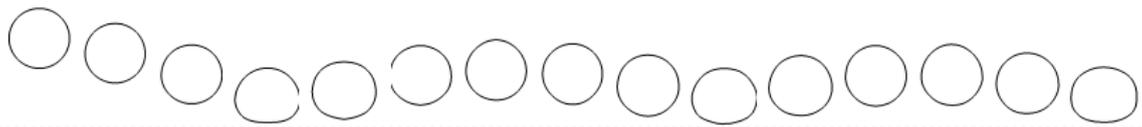
$$\frac{\partial \vec{\xi}(\vec{x}, t)}{\partial t} + H(\psi) \vec{u} \cdot \nabla \vec{\xi}(\vec{x}, t) = 0$$

Simulations of a solid in a fluid with wall contact

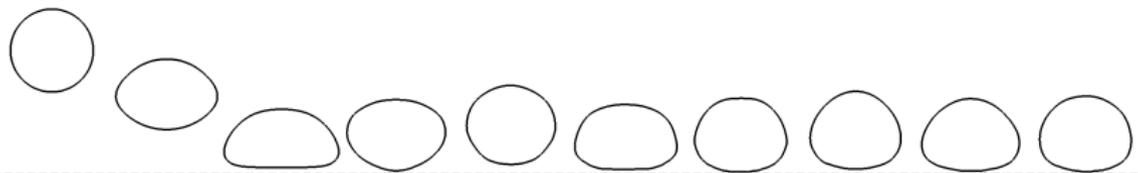
Collision in microgravity:



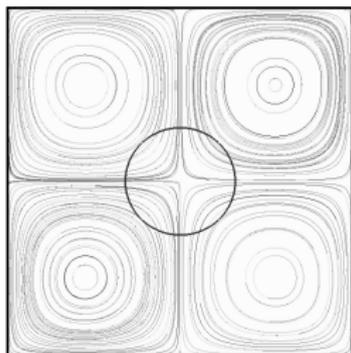
Collision in gravity - Stiff solid:



Collision in gravity - Soft solid:



Conservative vs Non-conservative formulation



Initial state

Non-conservative formulation:



Conservative formulation:



Conclusion

We here presented:

- An incompressible fully Eulerian formulation for soft solids in fluids using an approximate Projection method.
- Improvements to the previously proposed Reference Map Technique:
 - Momentum conserving formulation.
 - Non-dissipative schemes for flux computation - better KE conservation.
 - Momentum consistent solid advection.
 - An accurate and cost effective extrapolation procedure.
 - Use of collocated grids.

Future work:

- Analytical results for a quantitative comparison of fully coupled systems.
- An implicit formulation.
- Multigrid solver to speed up the poisson solution.

THANK YOU

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Reference:

Jain, S, S, & Mani, A, 'An incompressible Eulerian formulation for soft solids in fluids', *CTR Annual Research briefs*, 2017.

Reference map advection and Level-set reconstruction

Analytical expression for $\phi(\vec{x}, t = 0)$ is known.

Level-set reconstruction

$$\phi(\vec{x}, t) = \phi(\vec{\xi}, t = 0)$$

Reinitialize ϕ using Fast-marching method.

Modified advection equation

$$\frac{\partial \vec{\xi}(\vec{x}, t)}{\partial t} + H(\psi) \vec{u} \cdot \vec{\nabla} \vec{\xi}(\vec{x}, t) = 0$$

and

$$H(\psi) = \begin{cases} 1 & \Omega_S \\ 0 & \textit{else} \end{cases}$$

Advantages of this modification:

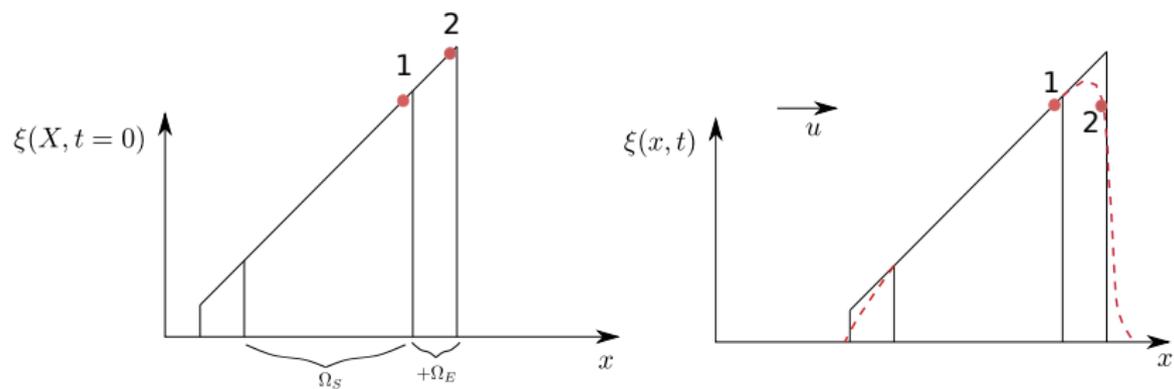
- removes high frequency content in $\vec{\xi}$ field - simple central schemes.
- robust solver.

[Jain & Mani, *CTR Annual Research Briefs*, 2017]

Comparison and updates on the recent approach

	<i>RMT15 (Valkov et al. 2015)</i>	<i>Present approach</i>
<i>Grid</i>	Staggered	Collocated
<i>Nature of the solver</i>	Compressible	Incompressible
<i>Reference map Extrapolation</i>	PDE based	Least-square based
<i>Level-set construction</i>	Advection in time	Reconstructed from $t = 0$ (Analytical - exact)
<i>Smoothing routines</i>	Required	No
<i>Discretization stencil</i>	one-sided	central
<i>Global damping</i>	Yes	No

Robustness due to modified advection equation



Solid-Solid contact

Define,

$$\phi_{12} = \frac{\phi^{(1)} - \phi^{(2)}}{2}$$

where $\phi_{12} = 0$ represents a midsurface between two solids.

Repulsive force

$$\vec{f}_{i,j} = \begin{cases} \gamma_{i,j} \hat{n}_{12i,j} & \phi^{(1)} < 0 \text{ or } \phi^{(2)} < 0 \\ 0 & \text{otherwise} \end{cases}$$

$$\gamma_{i,j} = k_{rep} \delta_s(\phi_{12i,j})$$

where $\hat{n}_{12i,j}$ is the unit vector normal to contours of ϕ_{12} and pointing away from the midsurface, k_{rep} is a prefactor and $\delta_s(x)$ is a compactly supported *influence function*,

$$\delta_s(x) = \begin{cases} \frac{1 + \cos \frac{\pi x}{w_T}}{2w_T} & |x| < -w_T \\ 0 & |x| \geq w_T \end{cases}$$